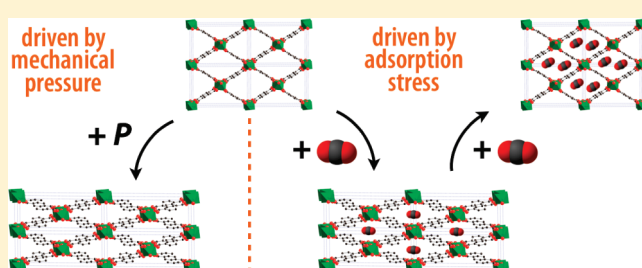


## Structural Transitions in MIL-53 (Cr): View from Outside and Inside

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Supporting Information

**ABSTRACT:** We present a unified thermodynamic description of the breathing transitions between large pore (lp) and narrow pore (np) phases of MIL-53 (Cr) observed during the adsorption of guest molecules and the mechanical compression in the process of mercury porosimetry. By revisiting recent experimental data on mercury intrusion and in situ XRD during CO<sub>2</sub> adsorption, we demonstrate that the magnitude of the adsorption stress exerted *inside* the pores by guest molecules, which is required for inducing the breathing transition, corresponds to the magnitude of the external pressure applied from the *outside* that causes the respective transformation between lp and np phases. We show that, when a stimulus is applied to breathing MOFs of MIL-53 type, these materials exhibit small reversible elastic deformations of lp and np phases of the order of 2–4%, while the breathing transition is associated with irreversible plastic deformation that leads to up to ~40% change of the sample volume and a pronounced hysteresis. These results shed light on the specifics of the structural transformations in MIL-53 (Cr) and other soft porous crystals (SPC).



The structural transitions in metal–organic frameworks (MOF) known as breathing have been attracting a lot of attention from both material scientists, who discovered and explored potential practical applications of this intriguing phenomenon, and theoreticians, who attempted to establish the thermodynamics foundations and simulation models to understand its physicochemical and mechanical mechanisms.<sup>1–5</sup> The most prominent breathing transitions were observed in the process of gas adsorption in some MOFs of the MIL-53 family. The MIL-53 framework is made of parallel one-dimensional M(OH) chains (M = Al<sup>3+</sup>, Cr<sup>3+</sup>), linked together by 1,4-benzenedicarboxylate (BDC) ligands to form linear diamond-shaped channels that are wide enough to accommodate small guest molecules.<sup>6–8</sup> This structure may oscillate (or “breathe”) between two distinct conformations called a large-pore phase (lp) and a narrow-pore phase (np; see Figure S1, Supporting Information), which have a remarkable difference in cell volume of up to 40%. The conditions, at which the breathing of MIL-53 happens, have been widely studied earlier, and it was shown in particular to be triggered by changes in temperature,<sup>9</sup> as well as adsorption of some gases and fluid mixtures at room temperature, but not others.<sup>10–14</sup> Recent work has been successful in rationalizing the conditions for the occurrence of breathing in MIL-53,<sup>15</sup> by considering the issue from the point of view of thermodynamics in the osmotic ensemble, which is the

statisticomechanical ensemble adapted for the study of adsorption in a flexible host.<sup>16</sup> This thermodynamic analysis was then extended to fluid mixtures and to an investigation of the temperature dependence, which allowed to predict complete pressure–composition and pressure–temperature phase diagrams for various adsorbates in MIL-53.<sup>17–19</sup>

Recently, the authors<sup>20</sup> suggested a rationale for breathing transitions driven by guest molecules adsorbed inside the pores. It was shown that the adsorbed molecules induce a significant stress inside the elastic framework that may be of the order of several to tens of MPa. This adsorption stress,  $\sigma_a$ , may be either positive or negative depending on the loading, and thus it may induce either framework expansion or contraction. The breathing transitions from lp to np phase and back were treated as spontaneous nonequilibrium transitions occurring upon developing a certain threshold stress  $\sigma^*$ , which the respective phase cannot withhold. On the basis of this adsorption stress model and the threshold stress ansatz, the authors described on a semi-quantitative level the breathing transitions driven by Xe and CH<sub>4</sub> adsorption on MIL-53 (Al).<sup>20,21</sup>

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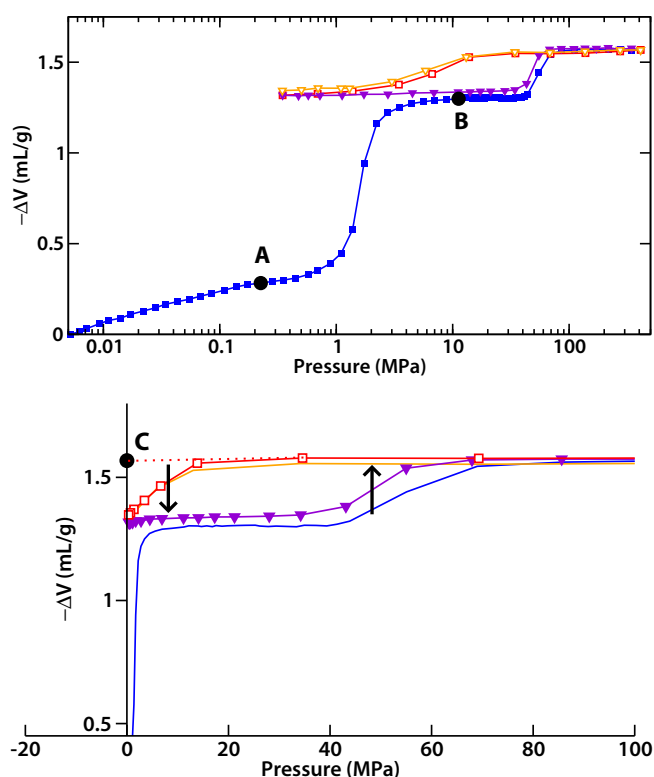
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In a recent publication, Beurroies et al.<sup>22</sup> demonstrated that the structural transitions between lp and np phases can be induced by uniform mechanical compression of the sample from outside in the process known as mercury porosimetry.<sup>23</sup> The powder of MIL-53 (Cr) particles was immersed into liquid mercury subjected to the external pressure. Upon the increase of pressure, mercury, being a nonwetting fluid, was forced to penetrate into interparticle voids of micrometer size, but it did not intrude into the internal pores of nanometer size, thus exerting a uniform pressure on the particles. The lp–np transition in the process of mercury intrusion and the reverse np–lp transition in the process of mercury extrusion occurred at significantly different pressures, giving rise to a pronounced hysteresis loop formed by intrusion–extrusion curves.

In this work, we extended the thermodynamic approach based on the osmotic ensemble<sup>16</sup> coupled with the adsorption stress model<sup>20</sup> suggested for the description of adsorption-induced breathing transitions, to describe mechanically driven transitions observed by Beurroies et al. with MIL-53 (Cr).<sup>22</sup> To this end, we revisited the mercury intrusion data and compared it with CO<sub>2</sub> adsorption and in situ XRD data collected on MIL-53 (Cr) by Serre et al.<sup>10</sup> We demonstrate that the magnitude of the adsorption stress applied inside the pores by adsorbed molecules, which is required for inducing the breathing transition, corresponds to the magnitude of the external pressure applied from the outside that causes irreversible plastic transformation between lp and np phases. This conclusion allows the prediction of the adsorption-induced phase transformations of MOF based on the mechanical contraction experiments.

## 1. VIEW FROM OUTSIDE: WHAT CAN BE LEARNED FROM THE MERCURY INTRUSION–EXTRUSION EXPERIMENTS?

In the mechanical compression experiments, a powder of MIL-53 (Cr) particles is placed in the sample cell of the mercury porosimeter, which represents a piston-cylinder assembly. To ensure that the particles are in the lp state, the sample was initially immersed in methanol which is known to open the MOF structure. Then it was outgassed at 150 °C to remove adsorbed species, cooled, and transferred as quickly as possible in the mercury porosimeter cell for analysis. In the mercury apparatus, a primary vacuum is set lower than 5 Pa. Then, a given amount of mercury is added into the sample cell on the top of the powder, and the mercury pressure is gradually increased by a hydraulic pump. The cell volume underneath the piston is measured as well as the equilibrium external pressure applied through the piston to the mercury and thus transmitted to the powder particles. The results of the mercury intrusion–extrusion cycles are presented in Figure 1. Note that the raw data<sup>22</sup> was corrected for the mercury compressibility and the pressure transducers hysteresis using blank calibration experiments on mercury intrusion–extrusion inside the empty sample cell. This correction is necessary for quantitative analyses of the experimental data at high pressures, especially in the region of hysteresis. The graph in Figure 1 gives the volume of mercury  $V$  penetrated at the given external pressure  $P$  into the volume occupied by the powder; the external pressure in the initial state is null,  $P = 0$ . The consecutive stages of the intrusion–extrusion process are shown by different colors: the blue curve depicts the primary intrusion obtained by raising  $P$  from 0 to 410 MPa, the red curve depicts the primary extrusion obtained by reverting the process at  $P = 410$  MPa and reducing  $P$  to 0.34 MPa, the violet curve depicts the secondary intrusion



**Figure 1.** Intrusion–extrusion experiments, featuring the volume variation of the sample ( $\Delta V$ ) as a function of mechanical pressure. Upper panel: logarithmic pressure scale; lower panel: linear pressure scale. Filled symbols for adsorption, empty symbols for desorption; squares for the first cycle, triangles for the second one. Remarkable points are as follows: A, the end of powder compaction upon compression; B, full interparticle filling upon compression; C, the hypothetical reference state of the np phase, corresponding to  $P = 0$ .

obtained by reverting the process at  $P = 0.34$  MPa and raising  $P$  again to 410 MPa, and finally the orange curve depicts the secondary extrusion obtained within the same pressure limits as the primary one. The almost ideal coincidence of the primary and secondary extrusion curves and colinearity of the primary and secondary intrusion curves at  $P > 10$  MPa show the reliability of the presented experiment.

The mercury porosimetry technique is a standard tool for pore size characterization of porous solids.<sup>23</sup> It employs the fact that being a nonwetting fluid, mercury penetrates into the pores only when the external pressure exceeds the capillary pressure determined by the Laplace–Washburn equation,  $P = 4\gamma \cos \theta / D$ , where  $D$  is the effective pore diameter,  $\gamma$  is the mercury surface tension ( $\gamma = 0.485$  N/m), and  $\theta$  is the contact angle, which for most solids varies from 130° to 145°.<sup>14</sup> Thus, in order to intrude mercury into micrometer-wide pores, the external pressure should exceed 0.2 MPa, and, respectively, filling of micropores ( $D < 2$  nm) may occur only at an external pressure exceeding ~600 MPa. These simple estimates help clarify the different steps in the mercury intrusion–extrusion cycle. The first step on the primary intrusion curve at low pressures  $P < 0.2$  MPa (Figure 1, point A) characterizes the powder compaction into a dense random packing without mercury penetration into the gaps between micrometer size particles of MIL-53 crystals. The second step, at  $0.2$  MPa  $< P < 10$  MPa (from point A to point B), reflects mercury filling of the interparticle voids in the dense

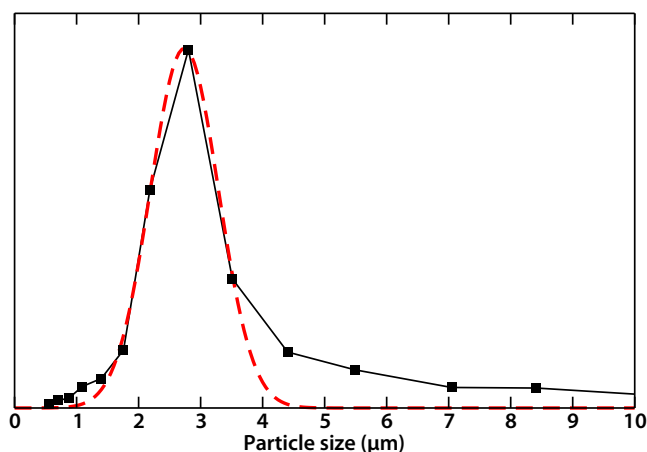


Figure 2. Particle size distribution (in black) and Gaussian fit (in red).

packing of particles without penetration into intraparticle pores. Indeed, the pores in MIL-53 are in the micropore range (<2 nm) and cannot be filled at pressures smaller than 600 MPa that exceeds the maximum pressure of 410 MPa achieved in given experiments.

**1.1. Particle Size Analysis** From the range of pressures, 0.2–10 MPa, corresponding to the interparticle filling, the particle size distribution can be estimated using the conventional method of Mayer and Stowe.<sup>24</sup> The calculated differential particle size distribution is presented in Figure 2 as the mass fraction of particles of given diameter. In the basic Mayer–Stowe equation,  $P = \kappa\gamma/D_p$ , which relates the intrusion pressure  $P$  and the particle diameter  $D_p$ , the mercury surface tension  $\gamma$  was taken as 0.485 N/m, and the dimensionless Mayer–Stowe constant  $\kappa$ , that typically varies in the range of 6–13, was taken as 10.<sup>25</sup> The average particle diameter is  $D_p = 2.7 \mu\text{m}$ , and the width of the distribution is  $\sim 0.8 \mu\text{m}$ . This is in agreement with the results of Khan and Jhung, where scanning electron microscopy (SEM) images showed relatively homogeneous particles of size 2–3  $\mu\text{m}$ , though on a different batch of MIL-53 particles.<sup>26</sup>

**1.2. Elastic Deformation and Bulk Modulus Estimate.** Neglecting mesopores, which may exist in small amounts due to possible defects and imperfections of MIL-53 crystals, we assume that mercury does not penetrate into intraparticle pores in the whole range of external pressures spanned in a given experiment. Upon the filling of interparticle pores, mercury exerts the uniform hydrostatic pressure on the particles and the further gradual increase of the intruded volume at  $10 \text{ MPa} < P < 35 \text{ MPa}$  reflects the elastic compression of particles, which are in the lp phase. This elastic compression should be reversible. From the slope of the intrusion curve in the region of linear elastic deformation, the volumetric elastic modulus (or bulk modulus)  $K_{lp}$  of the lp phase of MIL-53 crystals can be determined, as  $K = V_0 (\partial P / \partial V)$  with  $V_0$  being the reference volume of the respected phase. We have calculated the bulk modulus of the lp phase from the second mercury intrusion curve, for which the linear regime is clear (see Figure S2, Supporting Information). The value obtained is  $K_{lp} \sim 2 \text{ GPa}$ , which is in line with the values of bulk modulus reported in the literature for other MOF structures, which typically fall in the range 1.5–12 GPa.<sup>27,28</sup> (Note that HKUST-1 was reported to have a much higher bulk modulus than other members of the MOF family, at  $\sim 30 \text{ GPa}$ .<sup>29</sup>) Similarly, the bulk modulus of the np phase can be estimated

Table 1. Mechanical Parameters for the Two Phases of MIL-53 (Cr)<sup>a</sup>

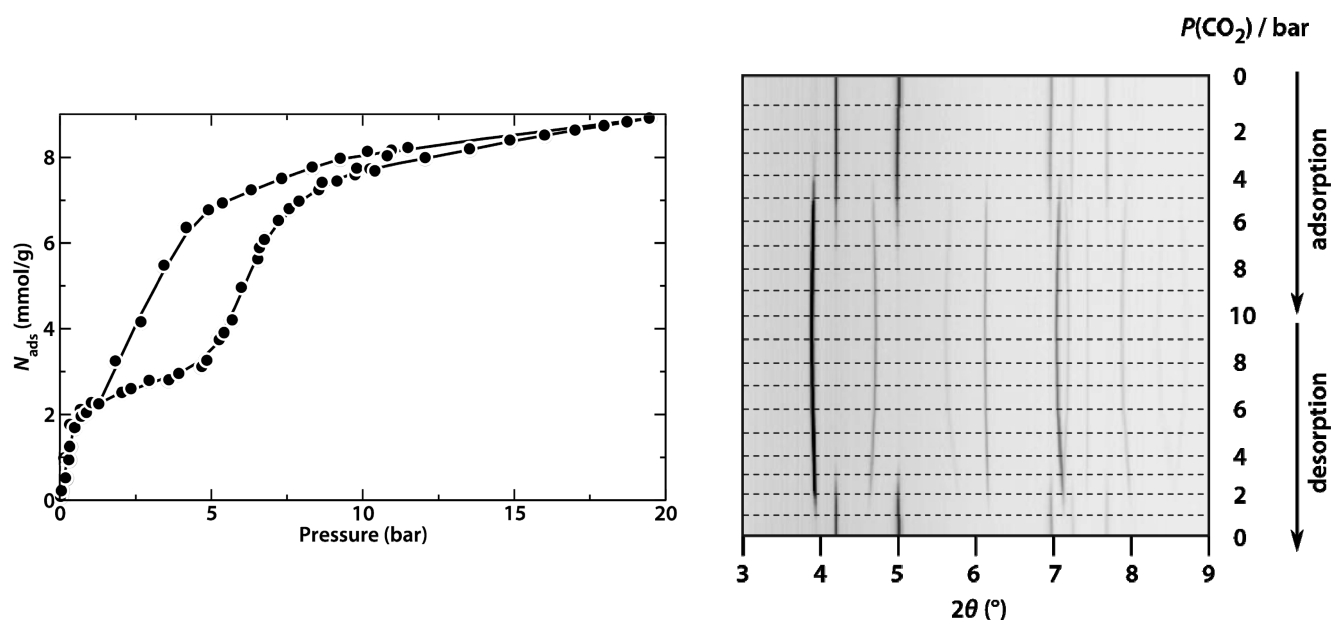
	lp phase	np phase
$V_0, \text{Å}^3/\text{u.c.}$	1486	1046
$P^*, \text{MPa}$	55 ( $\pm 15$ )	10 ( $\pm 10$ )
$K, \text{GPa}$	2	10
$\Delta V/V_0, \%$	2.7	3.6

<sup>a</sup>Reference state volume,  $V_0$ , as determined from crystallography; threshold stress ( $P^*$ ) and bulk modulus ( $K$ ) extracted from mercury intrusion–extrusion; relative deformation  $\Delta V/V_0$  during the mercury intrusion experiment,<sup>22</sup> calculated as  $\Delta P/K$  where  $\Delta P$  is the pressure range of existence of each phase.

from the primary and secondary extrusion curves, which overlap reasonably in the region of elastic deformation at  $P > 30 \text{ MPa}$ . Thus, the found value of  $K_{np} \sim 10 \text{ GPa}$  is larger than that of the lp phase. Indeed, the np phase, which is denser than the lp phase, is also less compressible. We can also estimate the elastic domain of deformation, i.e., the maximal variation of the crystal volume observed within the region of elastic deformation. The unit cell volume variation in the elastic regime for both phases is small (a few percent), as indicated in Table 1.

**1.3. Structural lp–np and np–lp Transitions.** The region of elastic contraction terminates with a prominent step at  $P^* \sim 55 \text{ MPa}$ , which was treated as the transition from the lp to the np phase. This transition is highlighted in Figure 1 with a vertical arrow. The volume of intruded mercury during this step, of  $394 \text{ Å}^3/\text{u.c.}$ , agrees within  $\sim 10\%$  with the difference in the volumes of lp and np phases as obtained from crystallographic data, namely  $440 \text{ Å}^3/\text{u.c.}$  The difference between these two values, of the order of 10%, may be ascribed to the continued existence of a fraction of lp phase in the experimental sample, as was observed upon Xe and  $\text{CO}_2$  adsorption.<sup>21,30</sup> According to the ansatz that the lp–np transition occurs upon achieving in the lp phase a certain threshold negative stress  $\sigma^*$ , the value of the external pressure  $P_{lp}^*$  of the lp–np transition gives the estimate of the maximum negative stress  $\sigma_{lp}^*$ , which the lp phase can withhold, namely  $P_{lp}^* = -(\sigma_{lp}^* - \sigma_{lp}^0)$ , where  $\sigma_{lp}^0$  is the prestress inherent to the dry material in the absence of mechanical constraint at  $P = 0$ . Moreover, the authors hypothesized that the threshold stress  $\sigma^*$  depends on the particle size, the smaller the particle the smaller the threshold stress.<sup>20</sup> Following this hypothesis, we can associate the width of the lp–np transition step  $P_{lp}^* = 55 (\pm 15) \text{ MPa}$  with the distribution of the threshold stress due to the particle size distribution. Thus, using the particle size distribution determined from the interparticle penetration region, the threshold pressure of the lp–np transition and the particle size can be correlated.

Upon further increase of pressure, the intruded volume increases linearly and reflects the elastic compression of particles, which are now in the np phase. The elastic compression is reversible as seen from the extrusion curve, which coincide with the intrusion curve within experimental errors. From the slope of the intrusion–extrusion curve in this region, the volumetric elastic modulus of the np phase can be determined. The elastic expansion of the np phase in the process of mercury extrusion terminates with a stepwise np–lp transition, which occurs in the range of pressures  $0 < P < 15 \text{ MPa}$ . Similarly to the lp–np transition, according to the threshold stress ansatz, the np–lp transition occurs upon achieving a certain threshold (now



**Figure 3.**  $\text{CO}_2$  adsorption and desorption isotherms at 304 K (left) and structural transformations upon adsorption followed by in situ XRD at 293 K (right). Figures are redrawn with permission from ref 10. Copyright 2007, Wiley-VCH Verlag GmbH & Co. KGaA.

positive) stress,  $P_{\text{np}}^* = 10 (\pm 10)$  MPa, which may depend on the particle size. The np–lp transition is, again, highlighted on Figure 1 with a vertical arrow.

Note that the external pressure in the intrusion experiment equals the negative stress calculated from the prestress in the reference evacuated sample at  $P = 0$ . For the lp phase, the situation is straightforward, since this reference state is the starting point of the intrusion experiment. However, the np phase of the MIL-53 (Cr) structure is unstable at the temperature of these experiments (around 300 K), so that no such reference state exists. To remedy the situation, we considered a hypothetical np state, which would be obtained by extrapolation of the linear elastic expansion regime down to  $P = 0$ , as the reference state for thermodynamic calculations. This extrapolation is shown in Figure 1 by a dotted line (lower panel; the reference state is marked as point C).

## 2. VIEW FROM INSIDE: ADSORPTION-DRIVEN STRUCTURAL TRANSITIONS

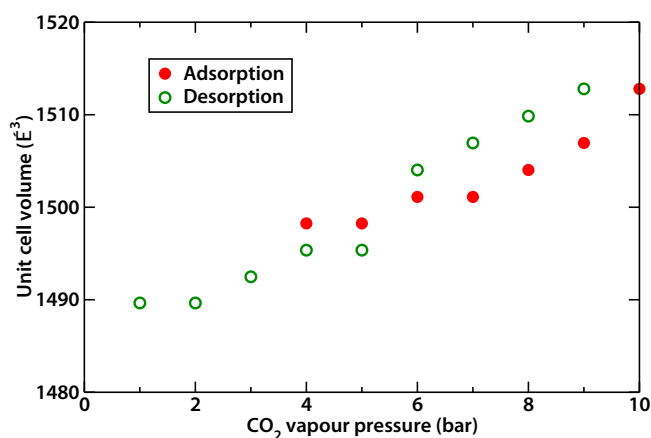
Gas adsorption was the first physical stimulus, for which breathing transitions in MIL-53 were observed, well before it was demonstrated that temperature and mechanical pressure could also trigger the lp–np structural transition. Adsorption of many gases inside MIL-53 (Al, Cr) is characterized by stepwise isotherms indicative of breathing transitions between np and lp phases, which occur at certain gas pressures depending on the nature of the guest molecules and the temperature. The criteria for observing the breathing phenomenon in terms of MIL-53 properties and fluid/solid interactions have been defined from the thermodynamic considerations. It was shown that breathing is a general phenomenon that occurs within a certain temperature range for all guest molecules.<sup>19,21</sup> Noteworthy, in the case of MIL-53 adsorbents, the two consecutive breathing transitions take place, lp–np at low gas pressure and np–lp at high gas pressure. The reverse lp–np and np–lp transitions occur in the process of desorption in a hysteretic

manner. Analyses of adsorption isotherms provide the quantitative information about the breathing transitions in terms of the difference of adsorption capacities of np and lp phases and, combined with in situ XRD patterns, the difference of unit cell geometries.

In the pioneering paper on  $\text{CO}_2$  adsorption in MIL-53 (Cr), Serre et al. reported in situ X-ray diffraction experiments performed during adsorption/desorption cycles at room temperature.<sup>10</sup> Revisiting this data on the adsorption-driven breathing obtained on the same structure as the mercury porosimetry experiments allows us to compare quantitatively the adsorption-driven structural transformations to those driven by mechanical pressure.

**2.1. Analysis of in Situ XRD Patterns.** The isotherms and pressure-dependent XRD patterns from ref 10 are reproduced in Figure 3 for one adsorption/desorption cycle. The step seen on the adsorption isotherm can be attributed to the np–lp transition, i.e., the second, high pressure breathing transition upon adsorption. The first, low-pressure lp–np transition happening around 0.3 bar<sup>31</sup> is not seen here. The evolution of the X-ray diffraction pattern upon adsorption and desorption shows a clear phase transition between the np and lp structures, respectively characterized by the peaks at  $2\theta$  around 5° and 3.9°. The transition can clearly be seen as a jump from one structure to another, with no intermediate XRD peak being observed. Moreover, it can be seen that, within a narrow range of pressure around the transition, the two phases can coexist in the experimental sample, as the two characteristic XRD peaks are observed simultaneously. Note that this does not necessarily mean the phase coexistence within one MIL-53 (Cr) crystal; in a powder sample, some crystals can be in the lp phase and the others in the np phase.

In addition, we also see that the position of the XRD peaks of each structure shifts slightly during adsorption, which is an indication of the elastic deformation of each phase. This deformation is due to the adsorption stress created by the presence of  $\text{CO}_2$  in the pores of the material. By using a simple geometric model of the MIL-53 flexibility, we were able to map these small



**Figure 4.** Unit cell volume variation for the lp phase upon CO<sub>2</sub> adsorption and desorption at 293 K.

displacements of the XRD peaks onto variations of unit cell volume. The details of this model (and equations) are given in Supporting Information.

The unit cell volume changes thus calculated are reported for the lp phase in Figure 4 (the plot for the np phase is less instructive as the amplitude of variations is much smaller). The relative variation of volume upon adsorption, of around 1.5%, is comparable to that measured from the mercury intrusion experimental data, indicating a good agreement between the two completely different sets of experimental results (and validating the geometric model used to process the XRD peak positions). Moreover, it can be noted that, because the measurements used for Figure 4 correspond to the high-pressure range of the adsorption and desorption isotherms, we are in a region of positive and increasing adsorption stress: as CO<sub>2</sub> pressure increases, more molecules are packed into the nanopores of MIL-53, leading to an outward stress. These experimental measurements are thus in agreement with the picture provided by the stress model proposed in our earlier work.<sup>20</sup>

**2.2. Analysis of the Adsorption Isotherms.** We have further applied the stress model<sup>20</sup> to the adsorption data presented in Figure 3 (left), combining the information we can extract from the adsorption isotherms with the data extracted from the mercury intrusion experiments, such as the bulk moduli of the lp and np phases and the values of threshold stresses corresponding the breathing transitions. All this information leads to a unique set of the parameters for the stress model of MIL-53 breathing, which are given in Table 1. It is noteworthy that, while we have previously used the stress model to provide for a qualitative understanding of the Xe- and CH<sub>4</sub>-driven breathing of MIL-53 (Al), introducing information from mechanical experiments has now enabled us to calculate quantitatively the actual adsorption stress in the material.

### 3. UNIFIED DESCRIPTION OF SAMPLE DEFORMATION ENGENDERED BY EXTERNAL PRESSURE AND ADSORPTION INSIDE THE PORES

The equilibrium elastic deformation of a porous solid immersed in a fluid (gas or liquid) thermostatted reservoir, which may contain one adsorbing species, is determined from the

following fundamental equation,

$$\begin{aligned} d\Omega(\mu, p_{\text{ext}}) &= d\left[F_s^0 + \frac{1}{2}K_0V_0^{-1}(V - V_0)^2 + p_{\text{ext}}V + \Omega_a(\mu, V)\right] \\ &= Nd\mu + Vdp_{\text{ext}} \end{aligned} \quad (1)$$

$$\Omega(\mu, p_{\text{ext}}) = F_s^0 + \frac{1}{2}K_0V_0^{-1}(V - V_0)^2 + p_{\text{ext}}V + \Omega_a(\mu, V)$$

where  $\Omega(\mu, p_{\text{ext}})$  is the osmotic ensemble thermodynamic potential of the combined solid+fluid system at the given external fluid pressure  $p_{\text{ext}}$  and chemical potential  $\mu$  of the adsorbate,  $V$  is the current sample volume,  $V_0$  is the sample volume in the evacuated (or “dry”) state at  $p_{\text{ext}} \rightarrow 0$  and  $\mu \rightarrow -\infty$ , which is considered as the reference state for thermodynamic analysis,  $F_s^0$  is the solid free energy in the dry state,  $K_0$  is the bulk modulus (or volumetric elastic constant) of the solid in the dry state, and  $\Omega_a(\mu, V)$  is the grand thermodynamic potential of the adsorbate at given  $\mu$  and  $V$ . Equation 1 implies that the changes of the solid free energy with respect to the dry state are accounted for by a harmonic elastic potential  $\frac{1}{2}K_0V_0^{-1}(V - V_0)^2$ . In this simplest consideration, we ignore a possible anisotropy of the solid and characterize the elastic deformation of the framework by the volumetric strain,

$$\varepsilon = \frac{\Delta V}{V_0} = \frac{V - V_0}{V_0} \quad (2)$$

The threshold stress ansatz implies that the regions of elastic deformations are limited by the minimum negative stress  $\sigma_{\text{lp}}^*$  and respectively minimum negative strain  $\varepsilon_{\text{lp}}^*$  in the case of lp phase and the maximum positive stress  $\sigma_{\text{np}}^*$  and respectively maximum positive strain  $\varepsilon_{\text{np}}^*$  in the case of np phase. According to linear elasticity in the vicinity of threshold points, the strain–stress dependencies for the lp and np phases are presented by two straight lines terminated at the threshold points, Figure 5. The slopes of these lines correspond to the respective bulk modulus  $K_{\text{lp/np}}$  of the lp and np phases. The mechanically driven transitions in the process of mercury intrusion–extrusion occurring upon achieving the threshold stress are depicted by the vertical lines in Figure 5. The resulting hysteresis loop is a mirror image of the experimental mercury intrusion–extrusion cycle in Figure 1 formed by the elastic deformation curves bounded by the vertical lines corresponding to the lp–np and np–lp transitions in the crystals of the mean size.

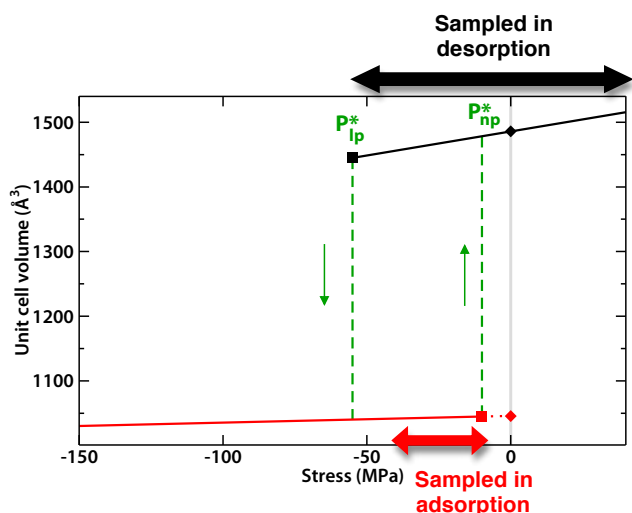
The equilibrium deformation is determined by minimization of the thermodynamic potential  $\Omega(\mu, p_{\text{ext}})$  with respect to the sample volume  $V$  at given  $p_{\text{ext}}$  and  $\mu$  that brings about a general relation between the volumetric strain  $\varepsilon$  and stress  $\sigma$  in the form of the Hooke law,

$$\sigma = K_0\varepsilon = \sigma_a - p_{\text{ext}} \quad (3)$$

Here, we introduced the adsorption stress,<sup>32,33</sup>

$$\sigma_a(V_0) = -\left(\frac{\partial\Omega_a}{\partial V}\right)\Bigg|_{\mu, V=V_0} \quad (4)$$

as the derivative from the grand thermodynamic potential with respect to the sample volume  $V$  at given external conditions of constant  $\mu$  and  $p_{\text{ext}}$ . Note that for one component fluid  $p_{\text{ext}}$  and  $\mu$  are related through the equation of state; that is in adsorption



**Figure 5.** Variation of the unit cell volume in the elastic regime, including threshold pressures and transitions, for both lp and np phases. The region of the stress–strain curves sampled during adsorption are also indicated.

experiments,  $p_{\text{ext}}$  equals the gas pressure  $p$ , and in the mercury intrusion experiments  $p_{\text{ext}}$  equals the applied pressure  $P$ .

Equation 3 constitutes the basis for a unified treatment of the mechanical and adsorption-driven deformation of MOFs. Indeed, the sample deformation in the process of adsorption should be similar to that in the process of mechanical compression provided the equality of the stress. We may conclude that assuming that both the adsorption experiment and compression experiment begin from the same initial dry evacuated state, the same sample deformation during adsorption and compression is achieved, when

$$P = -\sigma_a(\mu) + p \quad (5)$$

Equation 5 allows us to predict the adsorption-driven elastic deformation based of compression experiments, from which the stress–strain dependence (Figure 5) can be derived, and vice versa. This conclusion implies that the adsorption stress  $\sigma_a(\mu)$  can be calculated independently, for example, by employing an empirical Langmuir adsorption equation as it was done in our previous works for Xe and CH<sub>4</sub> adsorption on MIL-53 (Al).<sup>20,21</sup>

The variation of the cell volume of the MIL-53 (Cr) crystal in the process of CO<sub>2</sub> adsorption is a function of the adsorption stress.<sup>20</sup> Following our earlier treatment of Xe sorption in MIL-53 (Al), we approximated the adsorption isotherms on the lp and np crystals with the Langmuir adsorption equation,  $N(p) = N_0 K_H p / (N_0 + K_H p)$ , with the unit cell capacity  $N_0$  and the Henry constant  $K_H$  determined from the fitting of the experimental data.<sup>10</sup> The adsorption stress  $\sigma_a(\mu)$  was calculated according to eq 4, which in the case of Langmuir adsorption isotherm is directly related to the gas pressure,<sup>20</sup>

$$\sigma_s(p) = RT \left\{ \frac{dN_0}{dV_c} \left[ \ln(1 + K_H p / N_0) - \left( \frac{K_H p / N_0}{1 + K_H p / N_0} \right) \right] + \frac{dK_H}{dV_c} \left( \frac{p}{1 + K_H p / N_0} \right) \right\} \quad (6)$$

**Table 2. Model Parameters for Adsorption of CO<sub>2</sub> on MIL-53 (Cr) at 303 K<sup>a</sup>**

host structure	$K_H$ , bar <sup>-1</sup>	$N_0$	$dK_H/dV_c$ , bar <sup>-1</sup> Å <sup>-3</sup>	$dN_0/dV_c$ , Å <sup>-3</sup>
lp	2.7	9.3	$-5.5 \times 10^{-2}$	0.46
np	5.2	3.0	$-1.8 \times 10^{-2}$	$4.9 \times 10^{-3}$

<sup>a</sup> Langmuir parameters ( $K_H$  and  $N_0$ ) are taken from fitting the experimental data,<sup>10</sup> and their derivatives with respect to unit cell volume were optimized to reproduce the threshold stress corresponding to the lp–np and np–lp transitions in the mercury intrusion measurements (Figure 1) at the characteristic experimental pressures of the lp–np and np–lp transitions in adsorption measurements (Figure 3). Pressure transitions for the first transition, not visible in data from ref 10, were approximated to 0.2 and 0.3 bar, bracketing the experimental observations by calorimetry.<sup>31</sup>

In addition to  $N_0$  and  $K_H$ , the adsorption stress  $\sigma_s$  depends on the variations of these quantities with respect to the cell volume,  $dN_0/dV_c$  and  $dN_H/dV_c$ . It is noteworthy, that while  $dN_0/dV_c$  is apparently positive,  $dN_H/dV_c$  is in general negative. This gives rise to a nonmonotonic variation of the adsorption stress in the course of adsorption, as shown in ref 20. In the Henry region at low pressures,  $\sigma_s(p) \approx RT p dK_H/dV_c$  is negative and decreasing, that corresponds to the sample contraction. In the saturation region at high pressures,  $\sigma_s(p) \approx RT [dN_0/dV_c \ln(K_H p / N_0) + dK_H/dV_c (N_0 / K_H)]$  increases and may even become positive, leading to the sample expansion. Based on the threshold stress ansatz, the values of  $dN_0/dV_c$  and  $dN_H/dV_c$  were determined from eq 5, equating the characteristic mercury pressures of lp–np and np–lp transitions observed in the porosimetry experiments (vertical lines at the threshold pressures in Figure 5) and the adsorption stress (eq 6) of the respective transitions in the adsorption experiments (Figure 3, left). The parameters on the CO<sub>2</sub> adsorption isotherms on lp and np phases are given in Table 2.

Noteworthy, the system scans the different regions on the stress–strain diagram (Figure 5) during the adsorption–desorption cycle and during the intrusion–extrusion cycle. Indeed, in the compression experiments, the stress exerted by the external pressure is always negative, while the adsorption stress may be positive due to the packing effects at high loading. At the same time, the negative adsorption stress is limited in the adsorption experiments due to the competition between the guest–host attractive interactions and the repulsive guest–guest interactions. However, the most important conclusion is that in the process of external compression and in the process of adsorption, the host framework experiences the same strain–stress elastic behavior and the lp–np transitions occur upon achieving the same threshold stress, which can be either directly measured in the mechanical experiments or calculated from the adsorption isotherms.

#### 4. CONCLUSIONS: HOW SOFT ARE SOFT POROUS CRYSTALS?

In the recent literature, flexible MOFs which exhibit adsorption-driven elastic deformation, gating, and breathing phenomena, of which MIL-53 is one of the most characteristic examples, were named *soft porous crystals* (SPC).<sup>5</sup> Our study shows that *softness* of SPCs can be very different. Namely, one should distinguish between the structures such as the swelling MIL-88,<sup>34</sup> or interpenetrated dynamic frameworks,<sup>35</sup> which

change their volume gradually with respect to the applied stimulus of increasing magnitude, and the structures such as breathing MOFs of MIL-53 type considered here. These latter structures feature regions of small reversible elastic deformations within relatively wide ranges of variation of the stimulus terminated by large irreversible plastic deformations occurring in a stepwise manner, which lead to hysteretic phase transformations.

The mechanical compression experiments with mercury porosimeters provide not only qualitative but also valuable quantitative information about the mechanical properties of lp and np phases and the breathing transitions, including elastic modules of respective phases, the extent of the elastic deformation, and threshold stresses leading to the phase transformations, as well as the particle size distribution and correlations between the threshold stress and the particle size. The quantitative estimates extracted from the mercury porosimetry data on MIL-53 (Cr) samples correlate with the results of interpretation of the independent data on CO<sub>2</sub> adsorption isotherms and in situ XRD patterns collected in the process of CO<sub>2</sub> adsorption. The combined body of data from adsorption and mechanical experiments provides a solid foundation for a reliable theoretical consideration of the breathing transitions in SPCs.

The osmotic ensemble thermodynamic analysis based on the assumption of the additive contributions of the adsorption guest–host interactions and the host–host interactions treated within the framework of linear elasticity into the guest–host free energy allows the mechanically and adsorption-driven deformation of SPCs to be described in a unified manner. The adsorption stress exerted by the guest molecules adsorbed inside the pores causes the same framework deformation as the externally applied pressure of the same magnitude. The threshold stress ansatz implies that the lp–np structural transitions take place abruptly upon achieving the limit of elastic stability of the respective phase, similarly to the transition from elastic to plastic deformation. Noteworthy, while the volume changes between the lp and np phases of MIL-53 are quite substantial (~40%), the elastic deformations are limited to 2.7% (for lp) and 3.6% (for np). The coherent quantitative analysis of the lp–np transitions in MIL-53 (Cr) based on three types of measurements, mercury porosimetry, adsorption isotherms, and in situ XRD, confirms the validity of the proposed theory. The proposed thermodynamic treatment of adsorption deformation is not limited to ordered SPCs considered here and can be adopted to any compliant porous solids of different origin, ranging from zeolites<sup>32</sup> and mesoporous adsorbents<sup>36</sup> to coal seams in the process of carbon dioxide sequestration under geological conditions.<sup>37</sup>

## ■ ASSOCIATED CONTENT

**S** Supporting Information. Representation of the MIL-53 lp and np structures, fits used to determine the bulk moduli of the two phases, and detailed description of the geometrical model used for interpretation of in situ X-ray diffraction data. This material is available free of charge via the Internet at <http://pubs.acs.org>.

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