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Defects in metal-organic frameworks: a compromise between adsorption and stability?

A. W. Thornton, *^a R. Babarao, *^a A. Jain, ^{a,b} F. Trousselet^c and F.-X. Coudert^c

Defect engineering has arisen as a promising approach to tune and optimise the adsorptive performance of metal–organic frameworks. However, the balance between enhanced adsorption and structural stability remains an open question. Here both CO_2 adsorption capacity and mechanical stability are calculated for the zirconium-based UiO-66, which is subject to systematic variations of defect scenarios. Modulator-dependence, defect concentration and heterogeneity are explored in isolation. Mechanical stability is shown to be compromised at high pressures where uptake is enhanced with an increase in defect concentration. Nonetheless this reduction in stability is minimised for reo type defects and defects with trifluoroacetate substitution. Finally, heterogeneity and auxeticity may also play a role in overcoming the compromise between adsorption and stability.

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Introduction

Metal–Organic Frameworks (MOFs) or porous coordination polymers^{1,2} have emerged with promising properties for industrial applications such as chemical separation, storage, sensing and catalysis but their mechanical, thermal, chemical and hydro stability have remained poor.³

Defect engineering⁴ has arisen as an approach to further tune sorption, catalysis,^{5–7} band gap,⁸ magnetic⁹ and electrical/conductive properties. Wu *et al.* showed that defects enhance pore volume, surface area and CO₂ uptake.¹⁰ Ghosh *et al.* showed that CO₂ and H₂O uptake could be enhanced with the controlled location and concentration of defects.¹¹ Shearer *et al.*¹² and other studies have shown that the amount and type of defects can be controlled with the choice of modulators and synthesis conditions.^{7,13}

Defects are conventionally thought to reduce stability, however a few studies have shown that this depends on the type and nature of the defects. The stability of zirconium-based UiO-66 (and other UiO-series such as hafnium-based frameworks) has been attributed to the large number of coordination sites (*z*) per cluster, consisting of z = 12 compared to z = 6 for MOF-5 and z = 4 for ZIF-8 and HKUST-1.¹⁴ Defects

in the form of missing linkers or missing clusters would likely reduce the overall stability, however De Voorde *et al.* demonstrated that the replacement of a linker with a functional group (trifluoroacetate) improved the mechanical stability under ball milling treatment.¹⁵ Other studies have shown that defects can propagate to form defect planes in 2D across the whole dimension of the crystal as seen with fluorescence microscopy.¹⁶ Cliffe *et al.* further explored this correlation of defects and revealed the formation of nano-regions.¹⁷ Though the effect of heterogeneity on sorption and stability remains an open question.

No attention has yet been made on the balance between enhancement in adsorption *versus* the effect on stability with the introduction of defects. Sholl and Lively raised the question whether defects were a challenge or an opportunity.¹⁸ In the same spirit, the work presented here aims to understand the cost-benefit of defects by computationally exploring a systematic variation of defect concentration and type, introduced within UiO-66, see Fig. 1. Although the scope of possible defects is infinite, this controlled case study provides the opportunity to target and expose the isolated effects of modulator-dependence, defect concentration and heterogeneity, that are translatable to many other systems. Finally, carbon dioxide is chosen as the adsorbate of interest because of the global importance in reducing greenhouse gas emissions from fossil fuel-based power generators.¹⁹

Models and methodology

Materials

The fully activated structural model of UiO-66 in its hydroxylated form was constructed from the X-ray diffraction data



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^aManufacturing, Commonwealth Scientific and Industrial Research Organisation, Private Bag 10, Clayton Sth, VIC 3169, Australia.

E-mail: Ravichandar.Babarao@csiro.au, Aaron.Thornton@csiro.au

^bIndian Institute of Technology, Kanpur Nagar, Uttar Pradesh 208016, India

^cPSL Research University, Chimie ParisTech – CNRS, Institut de Recherche de Chimie Paris, 75005 Paris, France

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Fig. 1 Snapshot of calculations for stability and porosity on defective structures. Spatially-dependent Young's modulus *E* is shown to represent a measure of stability. Porosity available for adsorption is shown in blue for a probe diameter of 3 Å. Defects are shown from the perspective of a single cluster where additional linkers are consecutively removed, except for the reo structure that is also missing a cluster. Each missing ligand is replaced with either formate, acetate, chloride trifluor-oacetate or hydroxide ions. Each cluster is colored according to its coordination number: 12 - light blue, 11 - purple, 10 - dark blue, 9 - green and 8 - orange.

reported by Cavka *et al.*²⁰ UiO-66 consists of vertices (or nodes) represented by $Zr_6O_4(OH)_4$ clusters connected *via* linkers made of $C_6H_4(COO)_2$ ions or benzene-di-carboxylate (BDC). The Zr_6 clusters are 12-coordinated, and the framework is of the facecentered cubic type (fcu), with $F\bar{4}3m$ symmetry. The crystallographic cell of this structure is thus cubic, with cell parameters $a \sim 21$ Å. Since H atoms cannot be located from X-ray diffraction data, these atoms were added to the organic group and μ_3 -O position to neutralize the overall structure. For constructing defective UiO-66, the number of missing linkers per cluster was varied and compensated with the different capping ligands including formate, acetate, chloride, trifluoroacetate and hydroxide ions. Taking the example of formate (HCOO) capped ligands (or modulators), each defect consists of the replacement of a BDC ligand by two formate ions, at both endpoints of the linkage. For this modulator, five types of defective structures were considered at the unit cell scale (*e.g.* 4 clusters and 24 ligands for non-defective UiO-66). Defect positions were chosen so that the cluster coordinence is uniform and all missing linkers are if possible collinear, or at least coplanar:

(1) 1 defect at each cluster (2 per nominal cell), *i.e.* the cluster coordinence is z = 11 and the corresponding structure has P $\overline{4}3m$ symmetry.

(2) 2 defects at each cluster (such that all missing linkers in the cell are collinear), *i.e.* the cluster coordinence is z = 10 and the structure has *Imm2* symmetry.

(3) 3 defects at each cluster (all missing ligands are coplanar), *i.e.* the cluster coordinence is z = 9 and the structure has *Cm* symmetry.

(4) 4 defects at each cluster (all ligands in a given plane, say xy, are substituted), *i.e.* the cluster coordinence is z = 8 and the structure has *Imm*2 symmetry.

(5) 4 defects per cluster with a missing cluster (compared to the nominal structure). This corresponds to a framework called reo, and has $P\bar{4}3m$ symmetry. X-ray diffraction showed indications that this structure is more favourable than other structures with the same amount of defects.¹⁷

In addition, combinations of defects were considered, at the supercell scale (*i.e.* 64 clusters for non-defective UiO-66), for adsorption simulations only. Here six scenarios are generated where each supercell has an average of 9 linkers per cluster:

• Every cluster has exactly 9 linkers.

• Half of the clusters have 8 linkers and the other half have 10 linkers.

• Four scenarios where each supercell has 4 missing clusters (reo type defects) but with different degrees of adjacency from 1 to 4. Adjacency is defined here as the number of missing clusters directly adjacent from each other. For example, an adjacency of 2 means that there are 2 missing cluster sites directly next to each other.

Prior to performing adsorption simulations, geometric optimization were performed for the conventional unit cells of both the perfect and defective UiO-66 structures using Vienna *ab initio* simulation package (VASP)²¹⁻²³ with a plane-wave energy cut-off of 500 eV and a Gamma-point mesh for sampling the Brillouin zone. The density derived electrostatic and chemical (DDEC) method²⁴ was used to calculate the atomic charges based on a periodic unit cell for both perfect and defective UiO-66 structures using VASP software. However for the supercell scenarios, geometric optimization was performed using FORCITE module²⁵ based on the Universal Force Field (UFF)²⁶ due to the large computational cost.

Adsorption

The adsorption of pure CO_2 , and N_2 were simulated using the Grand Canonical Monte Carlo (GCMC) method. The adsorb-

ates were mimicked with a three-site model to account for the quadrupole moment. The C-O bond length in CO₂ was 1.18 Å and the bond angle ∠OCO was 180°. The charges on C and O atoms were +0.576e and -0.288e ($e = 1.6022 \times 10^{-19}$ C the elementary charge), resulting in a quadrupole moment of $-1.29 \times 10-39$ C m². The model reproduced the isosteric heat and isotherm of CO₂ adsorption in silicate.²⁷ N₂ had an N-N bond length of 1.10 Å, a charge of -0.482e on the N atom, and a charge of +0.964 at the center-of-mass, which were fitted to the experimental bulk properties of N₂.²⁸ Based on this model, the quadrupole moment of N_2 was -4.67×10^{-40} C m². The potential parameters were adopted from earlier work.^{29,30} The interactions of the gas-adsorbent and gas-gas were modeled as a combination of pairwise site-site Lennard-Jones (LJ) and Coulombic potentials. The LJ potential parameters of the framework atoms were adopted from the Dreiding force field and for the zirconium atom, the Universal force field (UFF)²⁶ was employed. The cross LJ parameters were evaluated by the Lorentz-Berthelot mixing rules.

The chemical potentials of the adsorbate in the adsorbed and bulk phases are identical at thermodynamic equilibrium, GCMC simulation allows one to relate the chemical potentials of the adsorbate in both phases and has been widely used for the simulation of adsorption. The framework atoms were kept frozen during simulation. This is because adsorption involves low-energy equilibrium configurations and the flexibility of the framework has a marginal effect, particularly on the adsorption of small gases.³¹ The LJ interactions were evaluated with a spherical cut-off equal to half of the simulation box with longrange corrections added; the Coulombic interactions were calculated using the Ewald sum method. The number of trial moves in a typical GCMC simulation was 2×10^7 , though additional trial moves were used at high loadings. The first 10⁷ moves were used for equilibration and the subsequent 10^7 moves for ensemble averages. Four types of trial moves were attempted in GCMC simulation, namely, displacement, rotation, and partial regrowth at a neighbouring position, and entire regrowth at a new position. Unless otherwise mentioned, the uncertainties are smaller than the symbol sizes in the figures presented.

The pore volumes of the adsorbents were obtained according to the thermodynamic method proposed by Myers and Monson.³² The UFF force field³³ was used to describe the LJ interactions of the framework atoms while the LJ parameters for helium were taken from the work of Talu and Myers.³⁴ The geometric surface area was calculated from a simple Monte Carlo integration technique where the centre of the mass of the probe molecule with a hard sphere is rolled over the framework surface. In this method, a nitrogen probe molecule was used to calculate the accessible surface area. Program poreblazer_V3.2 was used to calculate the geometric surface and pore volume.35 The accessible surface area was also calculated based on simulated N2 adsorption isotherms satisfying BET consistency criteria. ESI Table S1[†] shows the calculated geometric and accessible surface area, density and pore volume.

Stability

Complimentary to the adsorption simulations, the elastic constants were calculated for the defective structures, which were defined at the unit cell scale in the Materials section, to quantify the mechanical stability and softness. These calculations were based on DFT and performed with the Crystal14 software,³⁶ adapted to ordered solids as it deals with wave functions built on atom-centered functions (of Gaussian type), and efficiently uses translation invariance as well as point group symmetries. The basis sets used here are identical as those used previously.^{37–39} The *k*-point mesh is generated using the Monkhorst-Pack method.⁴⁰ To compute exchange and correlation contribution to the energy, a solid-state adapted exchange-correlation (XC) functional, named PBESOL0, was used - the latter was chosen because of its good performances in modelling cell parameters and mechanical properties of solids in general,⁴¹ and of non-defective UiO-66 in particular.

Within this computation scheme, each structure was first relaxed (both cell parameters and atomic coordinates, while keeping translational invariance and point group symmetries). Once an energy minimum was reached, elastic constants were calculated to quantify the mechanical stability and softness of the defective structures. Calculations were carried out by computing the energy variations subsequent to small deformations of the unit cell, following either of the 6 distinct deformation modes (3 for compression, 3 for shearing) for each mode, deformations corresponding to a strain of ± 0.01 were considered (along with the non-defective structure), and geometry optimizations at fixed strain were carried out (keyword used: ELASTCON).

For the elastic constants C_{ij} computed, minimal/maximal values of linear compressibility β , Young's modulus E, shear modulus G and Poisson's ratio ν were estimated, using the software Elate⁴² (available at http://progs.coudert.name/elate). Spatially-averaged quantities were also calculated based on the Hill's averaging scheme.⁴³

Results and discussion

Simulated CO₂ uptake within a range of defective structures except for the reo type is shown in Fig. 2. There are clear trends observed with the increasing number of missing linkers. At low pressures there is a general decrease in uptake with increased defect concentration. While at high pressures, the opposite trend is observed where an increase in uptake is observed with defect concentration. There is little variation in uptake amongst the structures with different modulators. Formate inhibits the uptake the most at low pressures (1 bar) while chloride helped maintain any loss in uptake. Uptake is sensitive to the interaction energy and surface area at low pressures while at high pressures the uptake is more correlated with pore volume.⁴⁴ In this case, structures with formatecapped defects exhibit the lowest surface areas and lowest pore volumes compared with the other types, which explains the lower uptake observed at high pressures (see Table S1[†]).



Fig. 2 Simulated CO_2 uptake at low (left) and high (right) pressures within a range of defective scenarios.

The effect of reo type defective structures is more interesting, see Fig. 3. A reo type defective structure is considered here with a missing cluster and an average of 8 linkers per cluster (note that the average number of missing linkers is dependent on the number of missing clusters per unit cell). For comparison, a structure also with 8 linkers per cluster but without a missing cluster is considered. The reo type defective structure consists of a large cavity of diameter 17 Å compared to the cavity diameter of 8.9 Å formed by only missing linkers, as shown in Fig. 1 and pore size distributions in Fig. S6 of ESI.† Interestingly the uptake is dramatically increased by more than double at large pressures for the reo scenario. This is impressive, but the question arises: do these enhancements come with a compromise in stability?

Note that the reo scenario investigated above considers the case of one missing cluster which represents a homogeneous case with equally spaced defects. In reality, the defects may be disordered or correlated. Here six scenarios are considered, see Fig. 4 with clusters color coded according to their coordination number. All six scenarios have an average of 9 linkers per cluster. For the first, every cluster has exactly 9 linkers. The second scenario has a combination of clusters with 8 and 10 linkers. The remaining scenarios are based on reo type defects where each cell has 4 missing clusters with varying degree of adjacency from 1 to 4. Adjacency is defined here as the number of missing clusters directly adjacent from each other. For example, an adjacency of 2 means that there are 2 missing cluster sites directly next to each other. The construction of these scenarios is an attempt to represent vacancy correlation, similar to that observed experimentally by Cliffe et al.¹⁷



Fig. 3 Simulated CO_2 uptake at high pressures within a reo type defective structure, a structure with 8 linkers per cluster on average and a perfect fcu structure.

Simulated CO₂ uptake is compared within all scenarios. For clarity, Fig. 4 depicts isotherms for only three scenarios. The isotherms within all reo type scenarios were almost identical. The dominant (most common) cavity size and pore volume remained unchanged which is why there no difference in the isotherms. Once again there is higher uptake observed within reo type defective structures compared to the missing ligand scenarios. There is a slight increase in uptake with less symmetry, *i.e.* the case of mixed clusters with z = 8 and 10. Pore size distributions in Fig. S6 of ESI,[†] show that the pore size shifts only from 8.6 to 8.9 Å from the perfect fcu structure.

Stability is analysed by considering the elastic constants generated from DFT-based simulations, as described in the Model and methodology section. It can be seen by the maximum and minimum elastic moduli in Table 1 for formate-modulated defective structures that, upon increasing the proportion of defects, anisotropy in mechanical properties is increased significantly. This anisotropy is amplified graphically in Fig. 1 and a closer view in Fig. S7 of ESI[†] for the Young's modulus. Covering the Young's and shear modulus, this increase is (in orders of magnitude) exponential with the defect number per cell n = 24 - 2z, with the corresponding anisotropy factors like $E_{\text{max}}/E_{\text{min}}$ reaching values >50 for z = 8. An exception is the reo structure, which is of much higher symmetry than the other defective structures.

Minimal Young's and shear moduli are obtained for axes playing a specific role in the structure, *e.g.* for z = 10 the



Fig. 4 (Top) Defect scenarios where all structures have the same average number of linkers per cluster (z = 9) and varying heterogeneity. Each cluster is colored according to its coordination number: 12 – light blue, 11 – purple, 10 – dark blue, 9 – green and 8 – orange. (Bottom) Simulated CO₂ uptake in three generalised scenarios: with symmetry, with lower symmetry and a combination of perfect fcu and defective reo.

Table 1 Minimal/maximal values of linear compressibility β , Young's modulus *E* and shear modulus *G* (all in units of GPa). Defective structures listed here are based on the formate modulator

Structure	β_{\min}	$\beta_{\rm max}$	E_{\min}	E_{\max}	G_{\min}	G_{\max}
fcu	7.91	7.91	45.18	54.62	17.10	21.27
<i>z</i> = 11	4.66	11.95	33.12	51.31	12.94	21.29
<i>z</i> = 10	-29.44	109.3	4.88	50.95	2.48	21.41
<i>z</i> = 9	-30.99	94.51	2.27	50.4	0.76	21.37
z = 8	-31.7	91.73	0.94	50.23	0.25	21.81
reo	16.94	16.94	22.52	27.28	8.60	10.75

easiest compression is in the direction parallel to missing linkers (X-axis, see Fig. S4 in ESI[†]) and the easiest shearing is that of the ($[10\bar{1}]^{\perp}$) plane along the [101] direction. Note that one observes negative linear compressibility (directions for which $\beta < 0$, *i.e.* along which the system contracts under uniform compression) and negative Poisson' ratio, for $z \leq 10$ (see ESI[†]).

This auxetic behaviour (compression along a given direction induces cell shrinking along a transverse direction) has been observed computationally in a number of MOFs including the 'wine-rack' series of MIL-140A, MIL-122(In), MIL-53(Al), MIL-53(Ga) and MIL-47,⁴² along with square-shaped DMOF-1⁴⁵ and the orthorhombic ZIF-4.⁴⁶ This property is thought to give rise to indentation resistance and fracture toughness.⁴⁷ This effect could also explain the defect-dependent increase in negative thermal expansion observed experimentally for hafnium-based UiO-66.⁴⁸

Modulator-dependent mechanical properties are considered here for structures with the same topology (z = 8 and z = 10) but with different substituents, namely formate (HCOO⁻), acetate (H₃CCOO⁻), hydroxyl (H₂O,HO⁻), chloride (H₂O,Cl⁻) and trifluoroacetate (F₃CCOO⁻) listed in Table 2. While the bulk modulus is almost insensitive to the nature of the substituent, concerning Young's and shear moduli one finds much more contrast between structures, which can be grouped in two sets.

On one hand, formate, hydroxyl and chloride substituents give values close to each other: $E \cong 18$ GPa, $E_{\min} \cong 0.8$ GPa, $G \cong 7$ GPa and $G_{\min} \cong 0.2$ GPa. Note the very small G_{\min} value while E_{\min} is about 4 times higher. Take for instance the formate-substituted structure (see Fig. S4-right†): here $(xy) = [001]^{\perp}$ is the plane common to all missing BDC's outgoing from a given cluster, so that each cluster has 4 outgoing BDC's in the $[110]^{\perp}$ plane and 4 in the $[1\overline{10}]^{\perp}$ plane. In this context, shearing can be exerted on *e.g.* $[110]^{\perp}$ without stretching the first group of ligands, and with minimal stretching ($\propto e^2$ with e the shearing strain) on the other ones. The very same mechan-

Table 2 Bulk modulus *B*, and spatially-averaged Young's modulus *E* and shear modulus *G* with minimal values (all in units of GPa). Four versions of z = 8 structures with different types of substitution ligands (or modulators) are listed. Values for formate (z = 10) and fcu structures differ slightly from those in Table 1, because of different convergence criteria in C_{ij} calculations

Modulator	В	Ε	E_{\min}	G	G_{\min}
8 linkers per cluste	er				
Formate	19.04	18.88	0.78	7.07	0.21
Acetate	17.33	25.18	7.56	10.01	2.73
Hydroxyl	17.64	18.24	0.85	6.87	0.23
Chloride	17.82	18.15	0.77	6.82	0.2
10 linkers per clus	ter				
Formate	22.82	30.53	4.85	11.95	2.47
Acetate	30.25	37.25	13.71	14.39	6.05
Trifluoroacetate	33.16	38.22	19.45	14.61	7.79
12 linkers per clus	ter				
fcu	42.13	50.61	44.98	19.47	17.01

ism makes compression easiest along the *x* and *y* axis (or their counterparts in the various structures, see axis 3 in Table 2). For comparison, in the non-depleted fcu structure, the 4 additional BDC's (absent here) would have been stretched proportionally to ε (2 elongated and 2 compressed), explaining the much higher (by 2 orders of magnitude) values of G_{\min} and E_{\min} – see for fcu in Table 1.

The other set contains acetate and trifluoroacetate-substituted structures. Here, Young's and shear moduli are much larger than for other substituents, by an order of magnitude. While G_{\min} still corresponds to the same kind of shearing, it is rendered less efficient (more costly) by the larger size taken by acetate and trifluoroacetate ions. Indeed, in the optimized structure methyl groups of both acetate ions replacing a missing BDC are relatively close to each other (H-H and C-C distances of about 2.5 Å and 3.3 Å respectively); this makes the repulsion between their corresponding electronic clouds nonnegligible, such that these ions can't be brought closer to each other as easily as in the case of e.g. formate substituents. Eventually the negative linear compressibility is observed or expected for all 5 types of substituents (along the direction normal to the plane of missing bdc's), the value $-\beta_{min} = |\beta_{min}|$ (not shown) is, however, about 3 times larger for small substituents than for acetate and trifluoroacetate, for the same reasons as discussed above.

In comparison, Fig. 5 displays the spatially-averaged constants along with simulated CO_2 uptake. The spatially-averaged mechanical constants are less dramatic in variation with the defect concentration compared with the change in minimum and maximum values from Table 1. The trend is rather expected, that the structures get softer (smaller *B*, *E* and *G*) when the number/concentration of defects increases. Furthermore, Young's modulus increases along with uptake at low pressure which could have important benefits for CO_2 capture separations.⁴⁹ For high pressures, the spatially-averaged Young's modulus decreases with increasing uptake, meaning that there is a compromise between uptake and stability. This is understandable given the general trend that missing linkers results in less structural support comprising mechanical stabi-



Fig. 5 Simulated CO_2 uptake at low (1 bar) and high (30 bar) pressures with Young's modulus as a function of defect types.

lity but also resulting in more pore volume that can enhance CO_2 uptake. Remarkably, reo type defective structures fight against this trend and offer a more stable structure coupled with an increase in uptake at high pressures.

While this study has covered a wide scope of defect scenarios there are many questions that still remain for future work. For example, the stability calculations are computationally expensive and incapable of exploring heterogeneity on a large scale such as the supercells described in Fig. 4. One can not take a simple average of elastic constants over a large scale. Heterogeneity is in itself a wide area of study which is covered here in a limited fashion. Effects of crystal edges are also not taken into account that have significant consequences on adsorption.⁵⁰ Furthermore, stability is treated here as independent of adsorption, which is likely to play a role. Nonetheless, this study merges multiple calculations of multiple scenarios in an attempt to bridge the gap of understanding on the compromise between adsorption and stability with defect engineering.

Conclusions

The role of defects on CO_2 adsorption capacity and mechanical stability was computationally explored. A systematic variation of defect types were considered including modulator-dependence (formate, acetate, hydroxyl, chloride and trifluoro-acetate), defect concentration (8 to 12 linkers per cluster and reo type defective structures with missing clusters) and hetero-geneity (adjacency of missing clusters).

 $\rm CO_2$ uptake at low pressures decreased as a function of defect concentration while uptake increased at high pressures. Uptake did not vary much with varying modulator, although chloride helped maintain any loss in uptake at low pressures.

Heterogeneity was explored by considering the level of adjacency among reo type defective structures. The correlation of defects did not affect the CO_2 uptake. However, the large cavities and pore volumes led to higher uptake than the perfect fcu structure.

The mechanical calculations revealed an especially interesting increase in anisotropy with defect concentration. In contrast, reo type defective structures were highly symmetric. Interestingly, acetate and even more so trifluoroacetate substitution was shown to strengthen the UiO-66 an order of magnitude above the other modulators.

Auxeticity (where a system contracts, under directional compression, in at least one transverse direction) was also observed for coordination numbers $z \le 10$. This effect could lead to superior indentation resistance and fracture toughness.

Finally, stability is compromised at high pressures where uptake is enhanced with an increase in defect concentration. However, reo type defective structures and structures capped with trifluoroacetate maintain relative stability above other type of defective structures.

In summary, stability is compromised when enhancing adsorption through defects but some stability can be main-

tained by engineering the type and distribution of defects. These results can be considered when designing defective structures for a wide scope of other adsorption applications such as hydrogen and methane storage.

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